Inelastic behaviour of cellulose microfibril networks

Srivatssan Mohan,^{a*} Gijsje H. Koenderink^b and Krassimir P. Velikov^{a,c,d*}

Supplementary Information

Note 1: Comparison of rheology for smooth and sand-blasted top plate to test for wall-slip effects.



Fig S1: Strain response of ϕ = 0.33 % CMF networks to an increasing and decreasing stress ramp, showing inconsistencies at different gap sizes when (a) a smooth top plate was used. A more uniform response was recorded with (b) a sand-blasted top plate, confirming the absence of wall-slip in this case.

Note 2: Determination of fractal dimension of single CMFs in DMSO.



Fig. S2: (a) 3D coordinates of single fibrils dispersed in DMSO traced in confocal image stacks using VAA3D.¹ (b) Esimation of fractal dimension from the length parameters of the traced fibrils (N= 50).

A dilute suspension (with a volume fraction of 0.01%) of CMFs in DMSO was sonicated using a bath ultrasonicator (Branson 8800, 40 kHz, 90 s) to disperse the fibrils. The suspension was then imaged in 3D in a 512 × 512 pixel format with an average voxel size of $80 \times 80 \times 200$ nm³, using a reflectance confocal microscope (Leica TCS SP8) in resonant scanner mode. We used a 100× NA 1.4 objective (n_{oil} = 1.515). From the volume image, the coordinates (with sub-pixel resolution) of the individual fibrils were obtained by semi-automatic tracing, using VAA3D software (version 3.20).¹ From the fibril coordinate data, both the fibril contour length (L) and end-to-end length (S) were obtained, from which a fractal

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dimension of 1.03 ± 0.03 was deduced, using the expression $S \propto L^{\overline{D_F}}$.²

Note 3: Constant maximum stress cycle using cone-plate geometry



Fig. S3: (a) Strain response of CMF networks (φ = 0.33%) to the application of stress cycles with a constant maximum of 8 Pa in a cone-plate measuring system at two different loading rates as indicated. (b, c) The recorded plastic and elastic component of the deformation with respect to the number of stress cycles.



Note 4: Cyclic constant linear strain ramp measurements

Fig. S4: (a) Constant maximum strain ramp protocol. (b) Stress response of ϕ = 0.33 % CMF network to the applied strain ramp at a strain rate of 1%/s. (c, d) The stress at the maximum applied strain of 100% (τ_{max}) and back at 0% strain (τ_{min}) at the end of every cycle, both shown as a function of strain cycles. (e) Dissipation energy which corresponds to the hysteresis loop area (normalized to k_BT) plotted as a function of the number of applied strain cycles.

References

- 1. H. Peng, Z. Ruan, F. Long, J. H. Simpson and E. W. Myers, *Nat. Biotechnol.*, 2010, 28, 348.
- 2. J.-M. Guenet, J. Rheol., 2000, 44, 947-960.